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Bolt Breakage Incident for Low-Level Radioactive Waste Container (1)

—Investigation into Cause and Measures—

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Abstract

The Nuclear Fuel Transport Co., Ltd. (“NFT”) found that lid anchor bolts (“lid bolts”) on Low-Level Radioactive Waste (“LLW”) containers failed during inspection and/or maintenance. LLW transport was suspended temporarily to verify LLW container safety after this incident. First, NFT went immediately to work to determine the cause and formulate measures to prevent any such recurrence. As a result, the cause was identified as “delayed fracture.” In addition, as for the recurrence prevention measures, we made the assessment that changing to a lower strength class of lid bolt would be effective. NFT resumed LLW transport using LLW containers for which recurrence prevention measures had been adopted.

Introduction

NFT owns over 3,000 LLW containers and has safely transported these for 25 years. An LLW container can be loaded with eight LLW drums (Fig.1). LLW is loaded into an LLW container, which is transported by the dedicated ship from a nuclear power station in Japan to Mutsu-Ogawara Port at Rokkasho Village. Then, it is transported by the LLW truck from the Mutsu-Ogawara Port to the disposal center. After the LLW is unloaded from the drum, the empty LLW container is returned to NFT’s LLW center where it is stored outside the center (Fig.2).

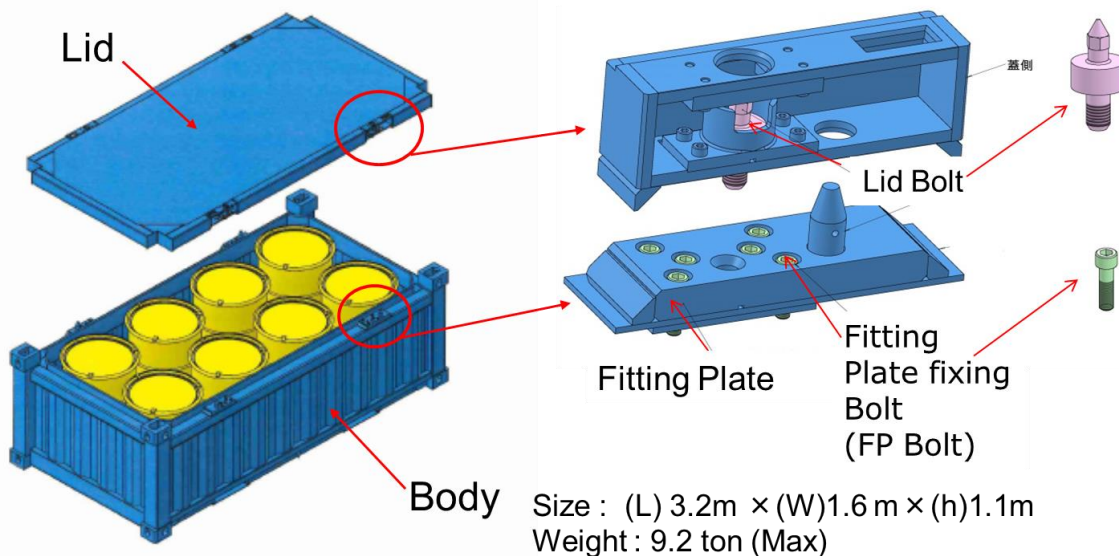


Fig.1 LLW container, fitting plate and lid bolts

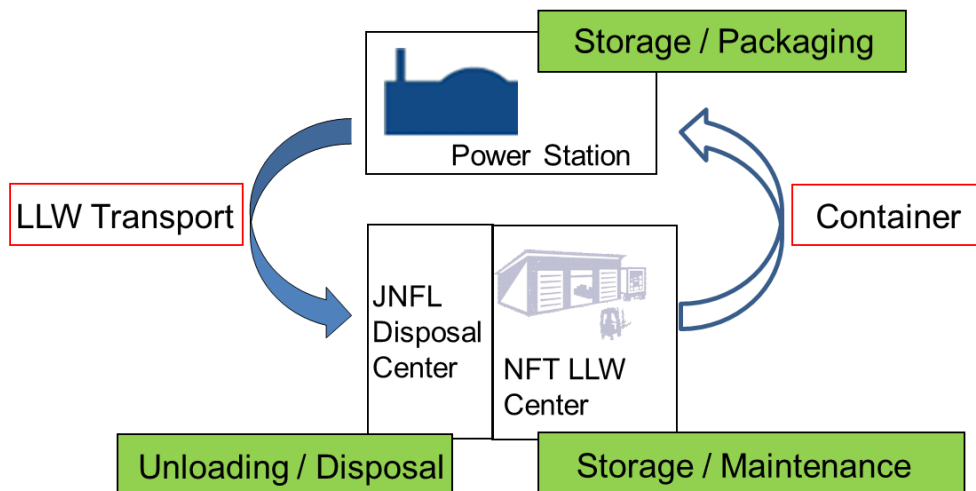


Fig.2 Cycle of LLW transport

Photo 1 shows a fractured lid bolt. A delayed fracture occurs without any sign under specific conditions. Accordingly, if such conditions are satisfied, all kinds of bolts may experience delayed fractures. Here, NFT presents a warning about delayed fractures and information about prevention measures.

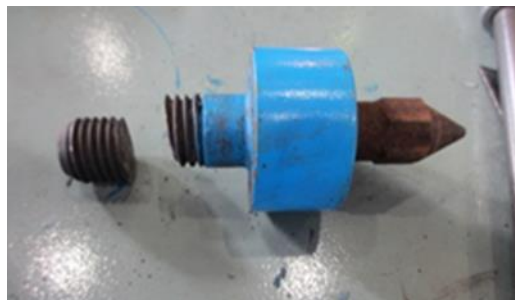


Photo 1 Fractured lid bolt

Lid Bolt Structure

The following is an overview of the lid bolt structure and conditions during transport and storage. Under normal use conditions, an excessive load is not placed on the lid bolts. However, when stored outside, water (ex. rainwater) can easily enter a tightened lid bolt.

1. Use conditions

Lid bolts are stored tightened onto all LLW containers at a torque of $147\text{N}\cdot\text{m} \pm 20\%$. An LLW container is used over a cycle of approximately one year. However, there are also containers that are not used for transport, but stored outside for one to two years.

2. Storage environment

In the case of outdoor storage, lid bolts are directly exposed to wind and rain (Photo 2). The arrows indicate the water intrusion route to a lid bolt.

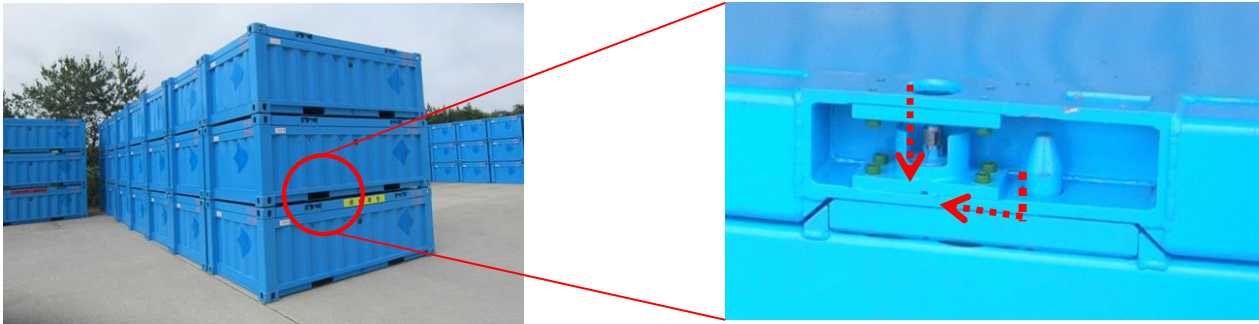


Photo 2 Transport containers stored outside at NFT LLW Center

3. Handling

A forklift and crane are used to move LLW containers. The corner posts are holded with the cell guides for transport by the dedicated ship. For LLW truck transport, the frame couples tightly to four mounting lugs on the bottom corners.

Bolt Breakage Incident for LLW Container

The first bolt breakage was conformed in February 2015. To date, a total of 16 fractured bolts have been confirmed. The characteristics of the containers on which bolts failed are as follows.

- Lid bolt strength class: 12.9 (equivalent tensile strength 1200MPa class).
- Lid bolts were tightened during transport/storage containers to the predetermined torque value.
- Some containers have never been used for transport.

Investigation into Cause

1. Fault tree analysis (FTA)

FTA of the lid bolt breakage was constructed using six factors: production, maintenance, operations, human factor, design and environment. The outcomes are shown in Table 1.

Table 1 Fault tree analysis results

| Factor | Point of view | Affairs / situation | Outcome |
|---------------|---|--|---------|
| Production | Manufacture, manufacturing lot | Passed inspection, no bias in the lot | N |
| Maintenance | Inspection, maintenance, repair | Performed as specified in manual | N |
| Operations | Handling, fitting, impact load, vibration during transport and handling | Torque value setting, no excessive load or vibration sustained | N |
| Human factors | During manufacture, storage and handling | Passed inspection, stored in a restricted access area | N |
| Design | Shape, material, corrosion resistance | Structure does not preclude contact with rainwater or other liquids, only strength class 12.9 bolts failed | Y |

| | | | |
|-------------|------------------------------|--|---|
| Environment | Outdoor storage, salt damage | Outdoor storage, structure does not preclude contact with rainwater or other liquids | Y |
|-------------|------------------------------|--|---|

2. Fracture surface observation

We examined the fracture surface of 16 broken lid bolts by the electron microscope. 15 lid bolts had an intergranular fracture that showed embrittlement.

Identification into Cause

Design and environment were specified as the causes of the breakages. For this reason, FTA was performed that was specific to the fracture mode of the lid bolts. As a result, the breakage was identified as due to delayed fracture (Table 2).

Table 2 Fracture mode review results

| Fracture mode | Occurrence factor | Bolt and container conditions | Outcome |
|-----------------------------|---|---|---------|
| Static fracture | ①Excessive torque setting ②Insufficient bolt strength | ①Continuous 147N-m \pm 20% (during storage and transport) ②Lid bolt is high-strength class (12.9) | N |
| | | | N |
| Fatigue fracture | ①Vibration ②Fracture surface of the shell pattern | ①Some containers have not been used for transport. ②Shell pattern was not confirmed | N |
| | | | N |
| Low-temperature brittleness | ①Environmental temperature and usable temperature of material ②Impact load | ①Environmental temperature: -5 °C practicable temperature of material: -20°C ②No impact damage to containers | N |
| | | | N |
| Stress corrosion cracking | ①Stress always applied ②Localized corrosion | ①Continuous 147N-m \pm 20% (during storage and transport) ②Ordinary rainwater does not result in stress corrosion cracking of carbon steel | Y |
| | | | N |
| Delayed fracture | ①High-strength bolts ②Water infiltration, embrittlement ③Load continually applied | ①Lid bolt used is high-strength class (12.9) ②Water enters the structure ③Continuous 147N-m \pm 20% (during storage and transport) | Y |
| | | | Y |
| | | | Y |

Review of Delayed Fracture Countermeasures

Delayed fracture is caused by a confluence of three elements (material strength, use environment and stress conditions). Accordingly, NFT measured the sensitivity to the amount of hydrogen in accordance with the strength class. From the results, we confirmed that the bolt breakage was caused by delayed fracture, and the effectiveness of the preventive measures (Fig.3). The strength class of the bolts was 12.9, which is close to the risky zone. Strength class 9.8 bolts are close to the safety zone and delayed fracture does not occur so easily. Therefore, it was concluded to be the adequate measure would be to lower the strength class of the material (12.9 ⇒ 9.8).

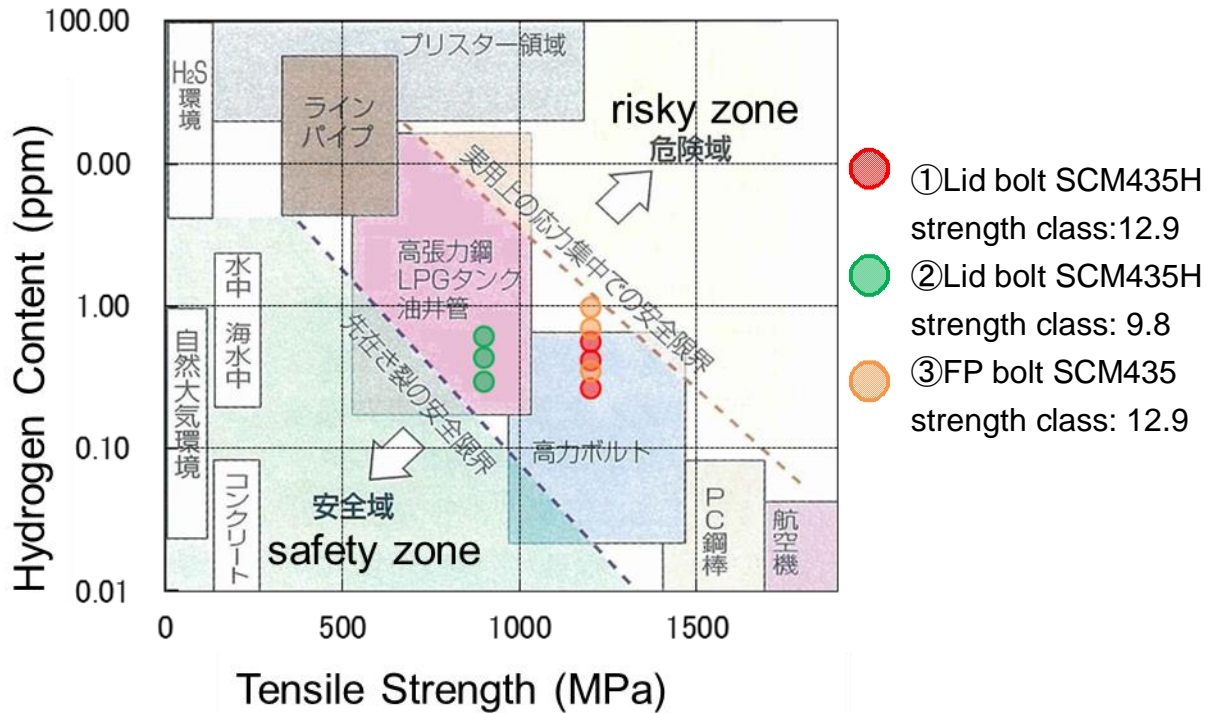


Fig.3 Plotted results of dissipative hydrogen content measurements (Plotted on references⁽³⁾)

Recurrence Prevention Measures

From the above results, the opinions of the taskforce and literature investigation, NFT concluded that changing of intensity classification would be a sufficient countermeasure. We implemented the following improvement measure to prevent any recurrence of this breakage.

- Modification of lid bolt material

Tensile stress class 12.9 ⇒ 9.8

- Lateral implementation

High tensile materials used for lid tightening were changed to a lower stress class.

FP-bolt material tensile stress class: 12.9 ⇒ 9.8 (Fig 4)

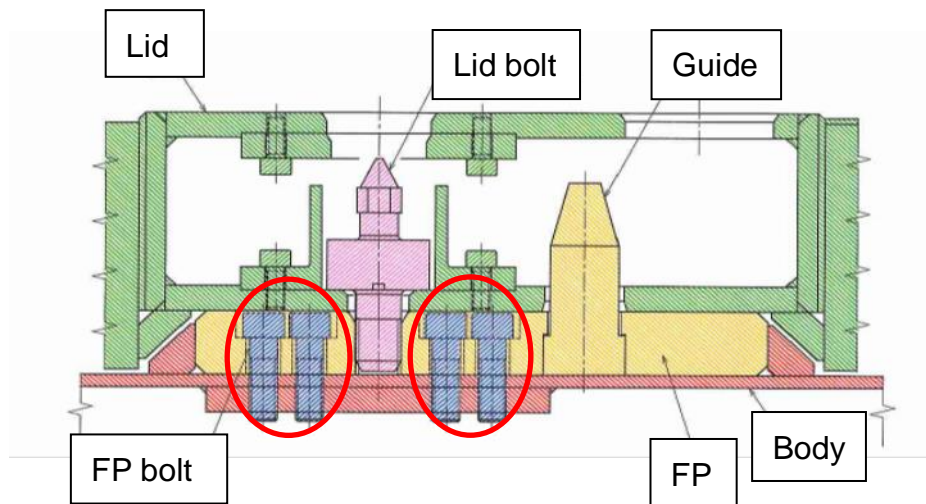


Fig 4 Overview of FP bolt

Conclusions

- ✓ Bolt breakages occurred due to “delayed fracture” which tends to happen to high-tension materials.
- ✓ NFT implemented the following improvement measures so that such breakages do not recur.
 - Modification of lid bolt material
Tensile stress class 12.9 ⇒ 9.8
 - Lateral implementation
FP- bolt material tensile stress class: 12.9 ⇒ 9.8
- ✓ NFT replaced the lid bolts and FP bolts at power plants and the LLW center in September 2015. We resumed transported using a transport vessel for which the measures were applied. No new bolts have failed, and the LLW containers have been safely transported.

References

- (1) Japan Society of Steel Construction, “Guidebook for Assessing the Characteristics of Delayed Fracture in High-Strength Bolts.”
- (2) Tanaka, Kazuaki, “Encyclopedia for Understanding the Fundamentals of the Latest Metals,” Shuwa System.
- (3) Matsuyama, Shinsaku, “Delayed Fracture,” Nikkan Kogyo Shimbun (1989).