





TNI Transportability Tool

A Software to Calculate the Transport Feasibility of Used Fuel Casks

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LOGISTICS

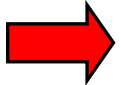


Context – Set of Problems – Stakes

▶ Transportation of nuclear materials: a risky activity

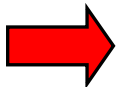
- ◆ Radioactive materials are close to the environment
- ◆ Many risks : accidents, terrorism, loss...

▶ Ways to prevent risks:



The cask itself

- shielding
- confinement
- sub-criticality



Reduce transport frequency

- optimise loadings in casks

Calculation Methods and Codes

- ▶ Use of **three-dimensional Monte-Carlo codes** coupled with **evolution codes** for all radioprotection calculations
- ▶ **Shielding calculations are composed of two evaluation steps**
 - ◆ radioactive sources
 - ◆ dose rates
- ▶ **Codes used at TNI for the evaluation of radioactive sources**
 - ◆ ORIGEN-2
 - ◆ ORIGEN-S
 - ◆ DARWIN-2 } for the irradiated fuel
- ◆ APOLLO-2 for the activation products on the fuel assembly ends

Calculation Methods and Codes

- ▶ Evaluation of dose rates around the cask are made with the three-dimensional Monte-Carlo code TRIPOLI-4
 - ◆ Calculation method without approximations
 - ◆ Three-dimensional geometry description
 - Eliminates approximation due to the modeling of the cask and content
 - Calculation in precise places such as trunnions
 - ◆ Detailed description of the sources (geometry and spectra)
 - ◆ Point wise cross section representation
- ▶ Calculation improvements are made without significant increase of computing time
- ▶ Using this method, the calculated dose equivalent rate values are **very close** to actual measurements around a package

Validation Process – Benchmarking

- ▶ The TNI shielding calculation method is validated by comparisons between the calculated and measured dose rates on casks
 - ◆ Several measurement experiments carried out on various casks
 - ◆ Full dose rate cartography around the cask when possible
 - ◆ Use of precise and well-calibrated instruments

Gamma-rays:

- Babyline

Neutrons:

- Cramal
- Berthold

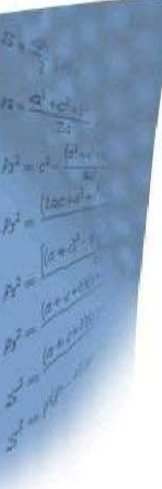


Validation Process – Benchmarking

- Summary of differences between measured and computed dose rates in the middle of the TN[®]112 cask in radial position

Position	Contact			2 metres		
	Measurements (10 ⁻² mSv/h)	Calculations (10 ⁻² mSv/h)	Differences* (%)	Measurements (10 ⁻² mSv/h)	Calculations (10 ⁻² mSv/h)	Differences* (%)
0°	8.97	9.52	+6.2%	2.44	2.60	+6.6%
45°	8.69	9.74	+12.0%	2.22	2.53	+14.1%
90°	9.23	9.62	+4.3%	2.83	2.54	-10.2%
135°	9.43	9.58	+1.6%	2.70	2.56	-5.2%
180°	9.13	9.51	+4.1%	-	2.57	-
225°	8.80	9.82	+11.7%	2.73	2.53	-7.5%
270°	9.23	9.50	+2.9%	2.88	2.54	-11.7%
315°	8.01	9.72	+21.4%	2.38	2.55	+7.1%
Average	8.94	9.63	+7.7%	2.60	2.55	-1.7%
Max	9.43	9.82	+4.2%	2.88	2.60	-9.7%
Min	8.01	9.50	+18.6%	2.22	2.53	+14.1%

* (calculated/measured -1) × 100%



Transportability A Software Tool

Transportability – Overview

- ▶ **Transportability is an internal software developed by TNI to manage: spent fuel assemblies, optimisation of loading plans, feasibility of transport**
- ▶ **Software functionalities**
 - ◆ **Inventory of the fuel assemblies per nuclear plant unit**
 - ◆ **Creation of loading plans in real time (fuel batch, position in basket)**
 - ◆ **Check of transport feasibility for a given date**
 - ◆ **Schedule earliest transport date for a given fuel batch**
- ▶ **Use**
 - ◆ **Transportability falls under the responsibility of the Calculation Department**
 - ◆ **Transportability is used by the shipping agents and sometimes by the customers**
 - ◆ **All transport scenarios are validated before expedition**

Transportability – Principles

▶ Transportability includes four steps:

- ◆ Input of data: the utility fuel assembly database
- ◆ Creation of a loading plan with the chosen fuel assemblies
- ◆ Choice of cask model, internal arrangements and transport date
- ◆ Calculation in two steps

Transportability – Addition of a Model

- ▶ The TN[®]112 can contain 12 MOX spent fuel assemblies per shipment

- ▶ The TN[®]112 will be input into Transportability following a **three-step method**
 - ◆ Modelling

 - ◆ Measurements

 - ◆ Model fitting

Transportability – Model Adjustment

► Methodology

- ◆ Determine the average ratio Measurements/Calculations
- ◆ Apply this ratio as a **factor** for each point
- ◆ Apply an additional **margin** to the gamma-ray and neutron dose rates to cover measurement uncertainties

► Example: Comparison between measured and computed dose rates at 2 metres from the TN[®]112 cask

Position	TRI3.79			TRI3.84		
	Measurements (10 ⁻² mSv/h)	Calculations (10 ⁻² mSv/h)	Ratio M/C	Measurements (10 ⁻² mSv/h)	Calculations (10 ⁻² mSv/h)	Ratio M/C
0°	1.92	2.03	0.948	2.44	2.73	0.893
45°	2.44	2.20	1.108	2.22	2.68	0.826
90°	2.46	2.27	1.083	2.83	2.73	1.037
135°	2.10	2.13	0.988	2.70	2.69	1.004
180°	-	2.13	-	-	2.73	-
225°	1.92	2.05	0.936	2.73	2.70	1.011
270°	2.10	1.93	1.088	2.88	2.74	1.051
315°	2.36	2.02	1.169	2.38	2.69	0.885

Transportability – Model Adjustment

► Example of model adjusting for the TN[®]112 cask based on two measurement experiments

- ◆ Calculation of the **average ratio** Measurements/Calculations to determine the adjustment factor for each point
- ◆ Application of an **additional 20% margin** to the gamma-ray and neutron dose rates to cover measurement uncertainties

► Results at 2 metres from the TN[®]112 cask in radial position

Position	Fitting Factor (ff)	Neutron Dose Rates (10 ⁻² mSv/h)	Gamma Dose Rates (10 ⁻² mSv/h)	Neutron × ff + 20%	Gamma × ff + 20%	Final tuned Dose Rates (10 ⁻² mSv/h)	Measurements (10 ⁻² mSv/h)	Differences (%)
0°	0.920	0.78	1.95	0.87	2.15	3.01	2.44	+23.7%
45°	0.967	0.79	1.90	0.91	2.20	3.11	2.22	+40.5%
90°	1.060	0.79	1.94	1.01	2.47	3.47	2.83	+22.7%
135°	0.996	0.79	1.90	0.94	2.27	3.22	2.70	+19.1%
180°	-	0.79	1.94	-	-	-	-	-
225°	0.974	0.79	1.91	0.92	2.23	3.16	2.73	+15.5%
270°	1.069	0.79	1.95	1.01	2.50	3.52	2.88	+22.1%
315°	1.027	0.78	1.91	0.97	2.35	3.32	2.38	+39.3%



Conclusion

Transportability is an innovative calculation tool

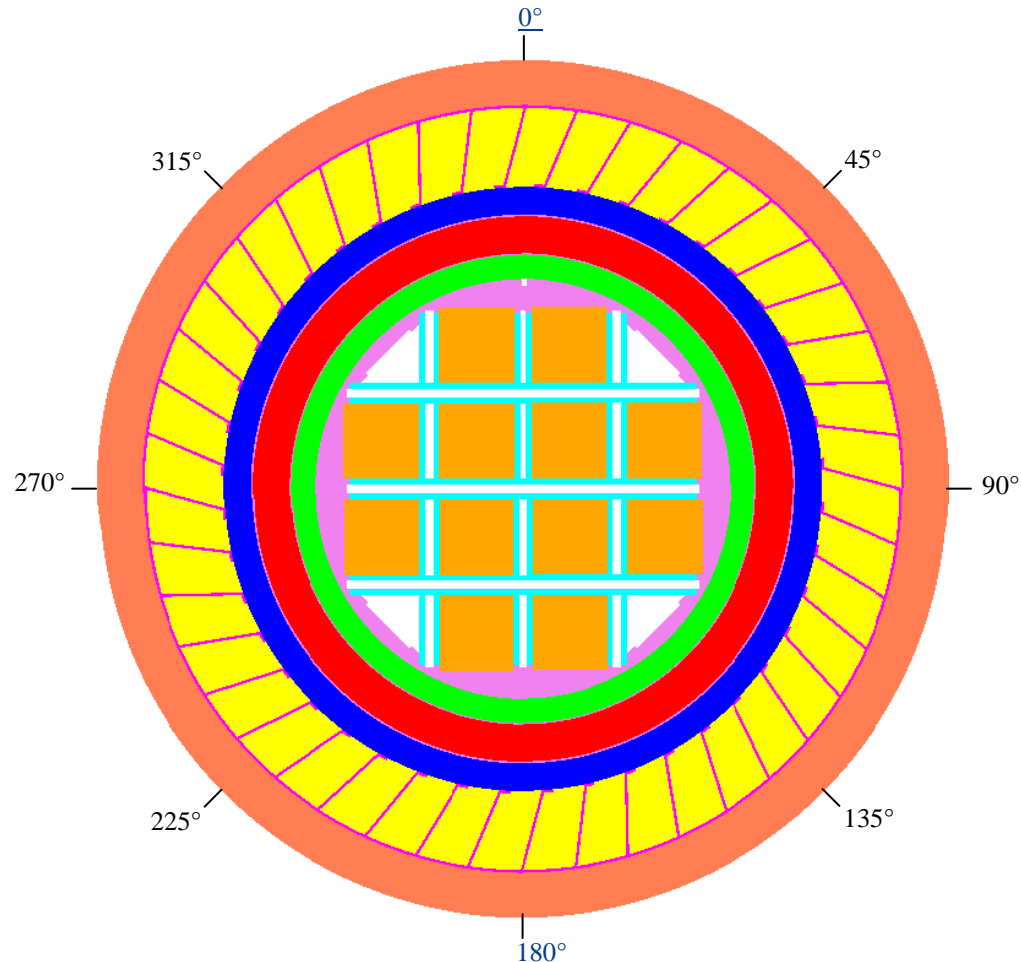
- ◆ Casks can be loaded with used fuel assemblies reaching 80% of the radioprotection criteria
- ◆ Radiological performance of the TNI transport casks is improved
- ◆ Increasing source intensities can be anticipated and compensated for
- ◆ General safety of the transport of radioactive materials is significantly enhanced



LOGISTICS

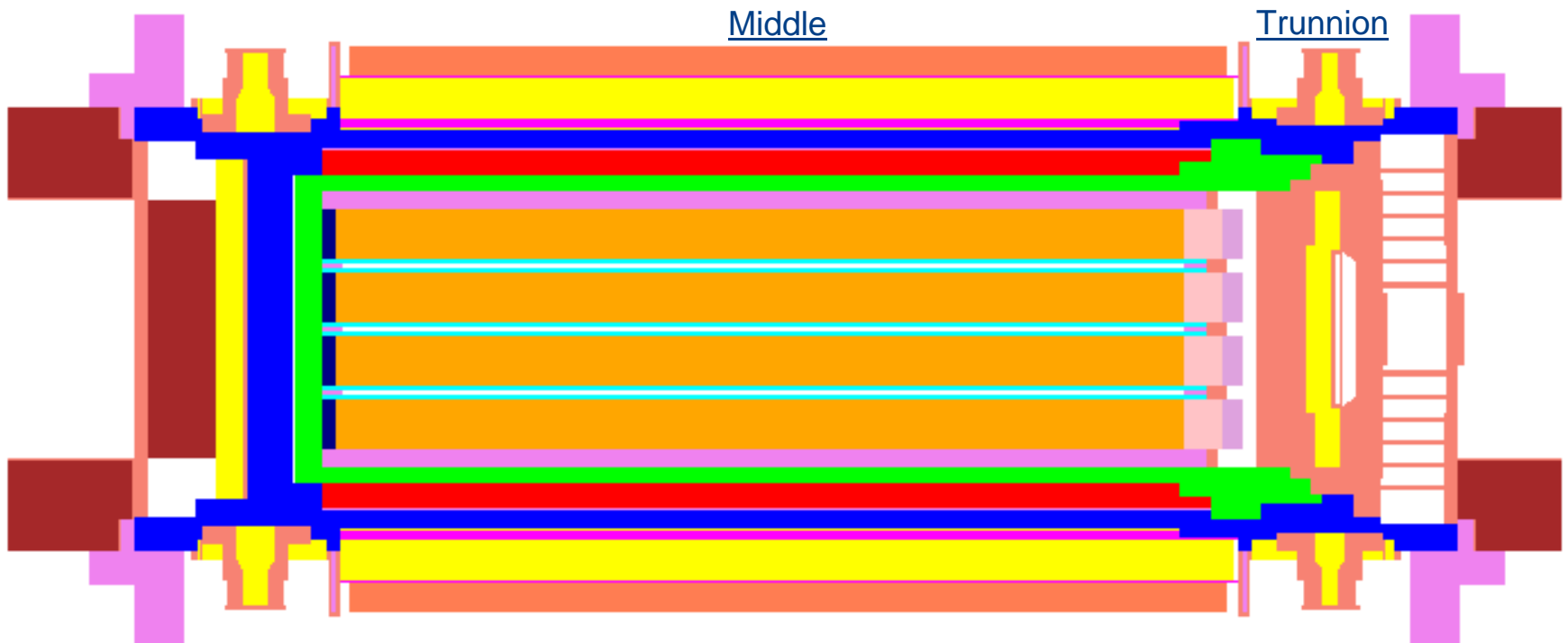
Calculation Methods and Codes

► TN[®]112 TRIPOLI 4.3 model: radial cross section



Calculation Methods and Codes

► TN[®]112 TRIPOLI 4.3 model: axial cross section



Transportability – Principles



Création d'un Lot

Lot	Référence ACL : <input type="text" value="Example_PATRAM"/>	Date du document : <input type="text" value="27/09/2010"/>
	Tranche : <input type="text" value="TRI3"/>	Référence Client : <input type="text"/>
	Créateur : Mikael DE BIASI	Date de création : 27/09/2010

Eléments combustibles disponibles : 678		Eléments combustibles affectés au Lot : 8	
<input type="radio"/> Non affectés <input type="radio"/> Affectés, non transportés <input type="radio"/> Transportés <input checked="" type="radio"/> Tous	<ul style="list-style-type: none">FX1JRMFX1JRNFX1JRPFX1JRRFX1JRTFX1JRVFX1JRWFX1JRXFX1JRZFX1JTAFX1JTCFX1JTD	▶	<ul style="list-style-type: none">FXP3MAFXP3MCFXP3MDFXP3MKFX139EFX139FFX139GFX139L
			<input type="button" value="Annuler"/> <input type="button" value="Valider"/>



Transportability – Principles



TRANSPORTABILITE

Consultation d'un Lot Service Calcul

Lot

Référence ACL : **Example_PATRAM** Date du document : 27/09/2010
 Référence Client :
 Tranche : **TRI3**
 Statut : **Créé**
 Créateur : **Mikael DE BIASI** Date de création : 27/09/2010

▲ Liste des éléments combustibles : [12]

Supprimer Modifier

EC	Combustible	U235 (%)	PU Métal (%)	Combustion (MW.j/t)	Activité (PBq)	Puissance Thermique (kW)	Intégrité	B3S	Transporté
FXP3MA	MOX	0,25	6,46	39261	51,83	7,67	Sain	Accepté	Non
FXP3MC	MOX	0,25	6,47	38750	51,43	7,58	Sain	Accepté	Non
FXP3MD	MOX	0,25	6,46	39346	51,76	7,64	Sain	Accepté	Non
FXP3MK	MOX	0,25	6,47	38761	51,19	7,56	Sain	Accepté	Non
FX1JRW	UOX	3,70	0	42225	18,70	1,97	Sain	Accepté	Oui
FX1JRZ	UOX	3,70	0	44603	11,88	1,06	Sain	Accepté	Oui
FX1JTC	UOX	3,70	0	44751	19,62	2,12	Sain	Accepté	Oui
FX1JTE	UOX	3,70	0	43021	11,43	1	Sain	Accepté	Oui
FX139E	UOX	3,71	0	46819	9,67	0,83	Sain	Accepté	Oui
FX139F	UOX	3,71	0	47432	9,79	0,85	Sain	Accepté	Oui
FX139G	UOX	3,71	0	47648	9,82	0,85	Sain	Accepté	Oui
FX139L	UOX	3,71	0	44049	9,85	0,83	Sain	Accepté	Oui

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LC

▼ Plans de chargement : [0]

Nouveau



Transportability – Principles



Création d'un plan de chargement

Plan de chargement

Référence : Loading_PATRAM

Tranche : TRI3

Lot : Example_PATRAM

Créateur : Mikael DE BIASI

Date du document : 27/09/2010

Date de création : 27/09/2010

Constitution du chargement : Optimiser le chargement

Activité	Puissance thermique	EC	27/09/2010	EC	Puissance thermique	Activité	
18,7 PBq	1,97 kW	FX1JRW [UOX]		FX139L [UOX]	0,83 kW	9,85 PBq	
51,83 PBq	7,67 kW	FXP3MA [MOX]		Vide			
9,82 PBq	0,85 kW	FX139G [UOX]		Vide			
		Vide		FXP3MA [MOX]			
		Vide		FXP3MC [MOX]			
		Vide		FXP3MD [MOX]			
		Vide		FXP3MK [MOX]			
		Vide		FX1JRW [UOX]			
		Vide		FX1JRZ [UOX]			
		Vide		FX1JTC [UOX]			
		Vide		FX1JTE [UOX]			
		Vide		FX139E [UOX]			
		Vide	FX139F [UOX]				
		Vide	FXP3MD [MOX]		2,12 kW	19,62 PBq	
		Vide	FX1JTE [UOX]		0,85 kW	9,82 PBq	

Annuler Valider

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Transportability – Principles



Calculs de puissances thermiques et/ou de débits de dose

Plan de chargement : **Loading_PATRAM**
 Lot : Example_PATRAM
 Tranche : TRI3
 Créateur : Mikael DE BIASI
 Date de création : 27/09/2010

Date : 01/01/2012

Emballage : TN12/2B

Panier : 927

Sélectionnez
 TN12/2A
 TN12/2B

Calculs thermiques

Calculs DED

Critère de transport : EDF-(Kam)-TN12/2-B-927 MOX-EC sains-nor								Modèle : TN12/2B 927 A SEC F		
par EC MOX		par EC UOX		par 1/4 secteur		par colis		Contact	1m	2m
Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Max.	Max.	Max.
	5,27		5,27				63,4	2		0,1

Annuler Valider



Transportability – Principles

Image des plans de coupe :

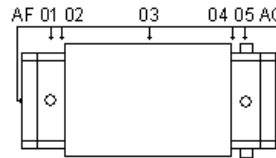
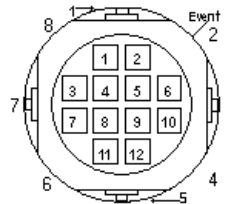


Image d'une coupe radiale :



Réponses unitaires gamma :

↑ Réponses unitaires neutron et gamma de capture :

	A	B	C	D	E	F	G	H
1	II° EC	II° Plan	II° Point	Distance	Fission spontanée Neutron	Fission spontanée Gamma de capture	Alpha II neutron	Alpha II gamma de capture
2	1	AC	1	0	1,17665E-03	8,99975E-04	1,46731E-03	1,01690E-03
3	1	AC	1	1	3,36705E-04	2,77061E-04	4,21675E-04	3,12541E-04
4	1	AC	1	2	1,33421E-04	1,57610E-04	1,67484E-04	1,77885E-04
5	1	AF	1	0	1,17966E-02	4,06852E-03	1,40296E-02	4,30457E-03
6	1	AF	1	1	3,58696E-03	1,13816E-03	4,27392E-03	1,20137E-03
7	1	AF	1	2	9,96090E-04	5,26197E-04	1,18771E-03	5,55095E-04
8	1	1	1	0	1,53880E-02	8,91777E-04	2,07976E-02	9,47331E-04
9	1	1	1	1	2,01069E-03	3,58514E-04	2,71879E-03	3,80549E-04
10	1	1	1	2	8,68474E-04	3,17546E-04	1,17584E-03	3,37042E-04
11	1	1	2	0	1,53880E-02	8,91777E-04	2,07976E-02	9,47331E-04
12	1	1	2	1	2,01069E-03	3,58514E-04	2,71879E-03	3,80549E-04
13	1	1	2	2	8,68474E-04	3,17546E-04	1,17584E-03	3,37042E-04
14	1	1	3	0	1,53880E-02	8,91777E-04	2,07976E-02	9,47331E-04
15	1	1	3	1	2,01069E-03	3,58514E-04	2,71879E-03	3,80549E-04
16	1	1	3	2	8,68474E-04	3,17546E-04	1,17584E-03	3,37042E-04

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LOGISTICS

Supprimer Modifier Rendre applicable Fermer

Transportability – Principles

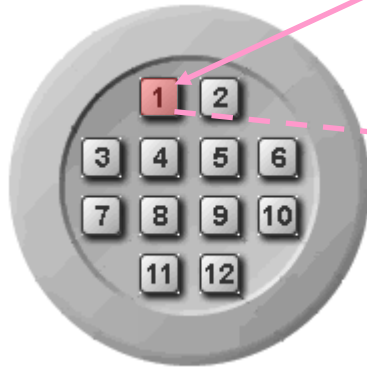
► 1st assembly:

Data base

ORIGEN2

Thermal power : P_{th1}

Source: s_1



Calculation point

$$\times DER_1 = s_1 \times \text{UnitDER}_1$$

Transportability – Principles

► For the 12 assemblies:

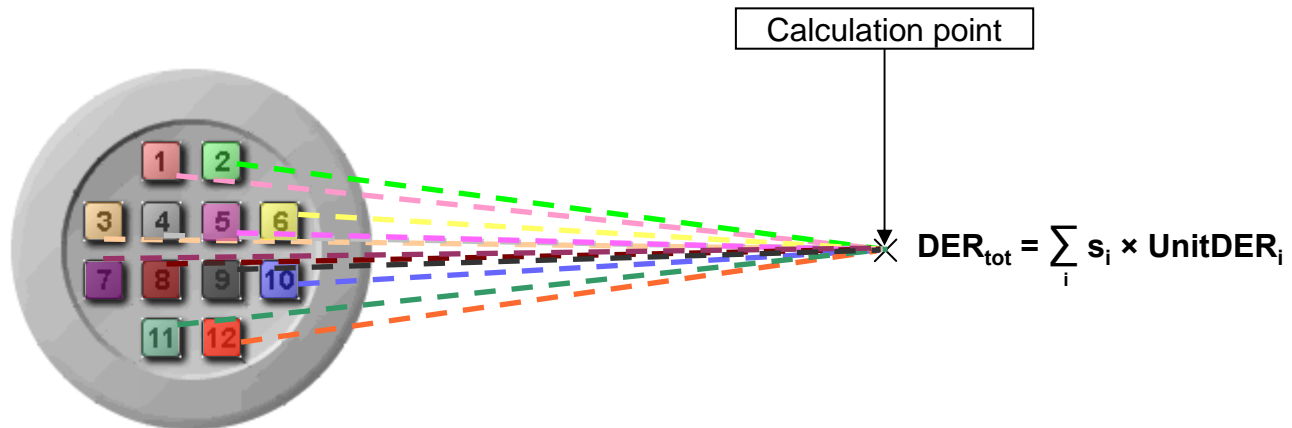
Data base

ORIGEN2

Thermal power of the loading

$$P_{th\ tot} = \sum_i P_{th\ i}$$

Sources: $s_1, s_2, s_3, \dots, s_{12}$



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