
Perturbation Analysis for Demonstration of Reactivity in Criticality Safety Analyses

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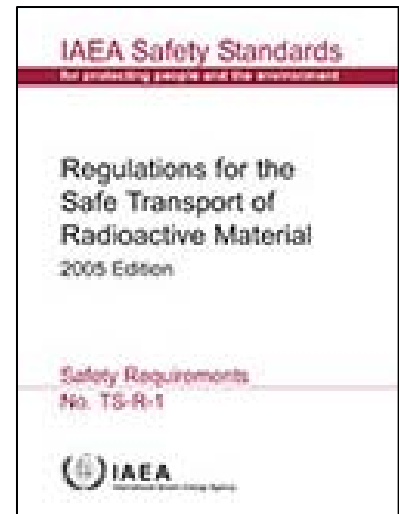
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Criticality Safety Analysis Guidance

- TS-R-1, paragraph 673

Where the chemical or physical form, isotopic composition, mass or concentration, moderation ratio or density, or geometric configuration is not known, the assessments of paras 677–682 [refer to the assessment of an isolated, individual package and package arrays for normal and accident conditions] shall be performed assuming that each parameter that is not known has the value which gives the maximum neutron multiplication consistent with the known conditions and parameters in these assessments.



Overview

- Perturbation Methods
 - Direct
 - Analytical
- Applications
 - Contents parameter selection
 - Burnable absorber rod distribution
 - Validation evaluations
 - Uncertainty analysis
 - Allowances

Perturbation Theory Benefit

- Evaluate the relative worth of a parameter
- Determine the sensitivity of the k_{eff} with respect to changes in the system
- Results in simplified contents specification
 - Minimize potential, unnecessary restrictions that transport package requirements would impose on the fuel bundle design
 - Simplify package approval document

Direct Perturbation Method

- Unknown parameter
 - varied and evaluated through complete calculation sets repeated
- Worth of variation determined by comparison

$$\rho_{worth} = \frac{k_{nominal} - k_{perturbation}}{k_{nominal}}$$

Analytical Perturbation Method

- Use of an analytical tool
 - SCALE sensitivity and uncertainty (S/U) analysis tool
TSUNAMI-3D
 - Calculates adjoint-based first-order linear perturbation theory sensitivity coefficients
 - Sensitivity Coefficient $\frac{\Delta k_{eff} / k_{eff}}{\Delta \Sigma / \Sigma}$
 - Validated by central difference direct perturbation



Applications

- Criticality safety transport analyses
 - Contents parameter selection
 - Burnable absorber rod distribution
 - Validation evaluations
 - Uncertainty analysis
 - Allowances

Contents Parameter: BWR Burnable Absorber (BA) Rods

- Background

- Burnable absorber rods within a BWR assembly are utilized to achieve desired core performance objectives

- Methodology

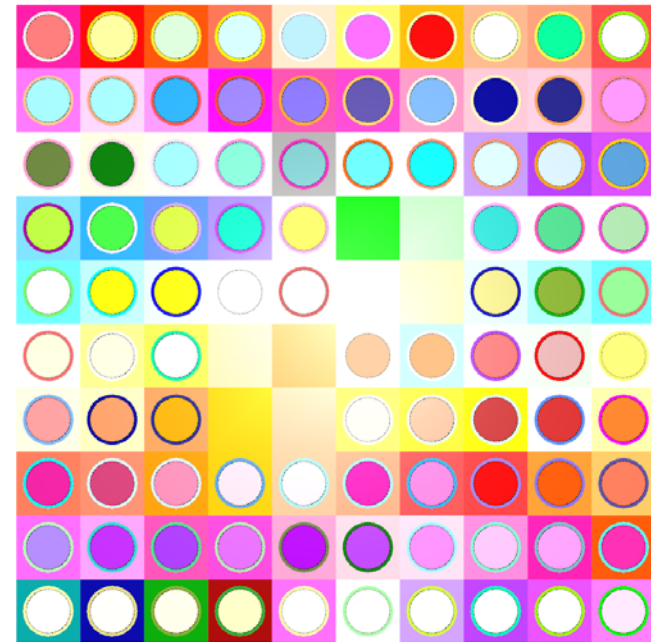


Burnable Absorber Rod Evaluation

- SCALE Models

- Each fuel rod 5.0 wt% enriched UO_2 + 0.1 wt% Gd_2O_3
 - Minimizes flux alteration
- Each fuel rod material has a unique material identifier
 - Accounts for individual location effects

- Sensitivity coefficients integrated over energy and region for ^{157}Gd



BA Rod Pattern Selection Example

- Identify least worth locations
- Symmetry rule
 - Calculate average worth among pairs
- Select pattern for criticality safety analyses



Least worth



Highest worth

Validation of Analytic Perturbation

Central difference
direct perturbation

$$S_{k,\alpha} = \frac{k_{\alpha+1\%} - k_{\alpha-1\%}}{k_{nominal}} \times \frac{100(\%)}{2x(\%)}$$

Case	Number Density Multiplier	Sensitivity Coefficient	Percent Difference
Fuel Rod	1 – nominal	-0.190 ± 0.0003	1.4%
	±10%	-0.192 ± 0.0004	
Infinite Bundle Array	1 – nominal	-0.115 ± 0.0013	10.7%
	±10%	-0.128 ± 0.0012	

Uncertainty Allowance Assessment

- Two allowance categories
 - (1) Analytical perturbation uncertainty
 - Material and fabrication tolerances
 - (2) Direct perturbation uncertainty
 - Geometric or material representation

Analytical Perturbation: Material and Fabrication Tolerances

- Reaction rate

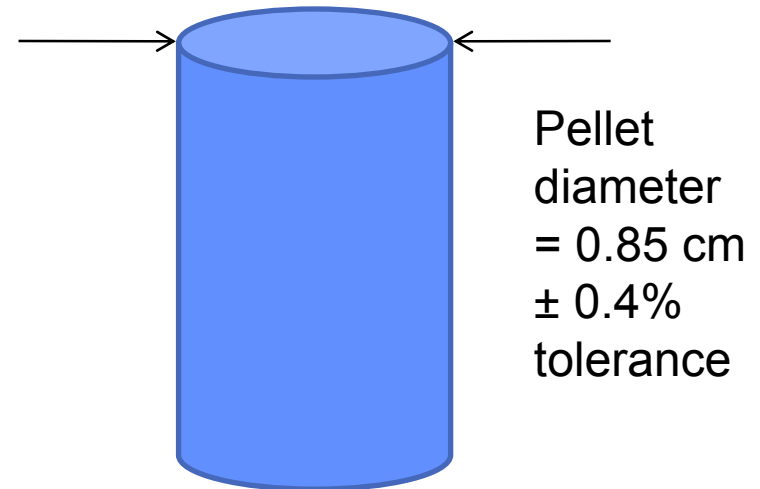
$$R = \phi \Sigma = \phi N \sigma \quad \Delta R = \phi \frac{N_A}{M} \Delta \rho \sigma = \phi N \Delta \sigma$$

- Sensitivity coefficient

$$\frac{\Delta k_{eff} / k_{eff}}{\Delta \Sigma / \Sigma} = \frac{\Delta k_{eff} / k_{eff}}{\Delta \rho / \rho}$$

- Tolerance correlation

$$-\frac{\Delta V}{V} \equiv \frac{\Delta \rho}{\rho}$$



Analytical Perturbation: Total Material and Fabrication Uncertainty

- Uncertainty associated with region

$$\left(\frac{\Delta keff}{keff} \right)_i = \left[\frac{\Delta keff / keff}{\Delta \Sigma / \Sigma} \right]_i \cdot \left(\frac{\Delta V}{V} \right)_i$$

- Simple summation

$$\left(\frac{\Delta keff}{keff} \right)_{TOTAL} = \sum_i \left(\frac{\Delta keff}{keff} \right)_i$$

- Analytical perturbation uncertainty total

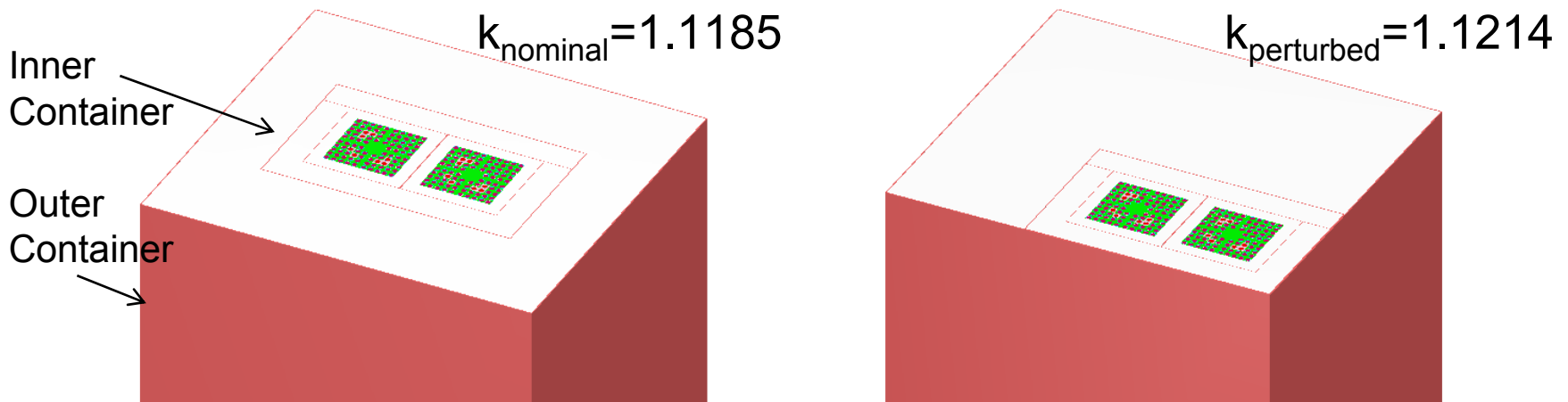
$$\Delta k_{u,analytical} = \left(\frac{\Delta keff}{keff} \right)_{TOTAL} \times k_p \quad \text{where } k_p = 1.0$$

Direct Perturbation: Geometric or Material Representations

- Direct difference between the nominal and perturbed case

$$\Delta k_{u,\text{direct}} = k_{\text{perturbed}} - k_{\text{nominal}}$$

- Example geometric representation: $\Delta k_{u,\text{direct}} = 0.0029$



Total Uncertainty

- Total combined uncertainty

$$\Delta k_u = \Delta k_{u,\text{analytical}} + \Delta k_{u,\text{direct}}$$

- (1) Analytical perturbation uncertainty

$$\Delta k_{u,\text{analytical}}$$

- Material and fabrication tolerances

- (2) Direct perturbation uncertainty

$$\Delta k_{u,\text{direct}}$$

- Geometric or material representation

Conclusions

Expanding the application of perturbation theory

- More efficiently define maximum k_{eff}
 - Simplify contents specification
- Use analytical perturbation method for evaluating BA rod position worth in a BWR lattice
 - Valid method of optimizing the contents parameters
 - Development of the uncertainty methodology shows relations between k_{eff} to nuclide density